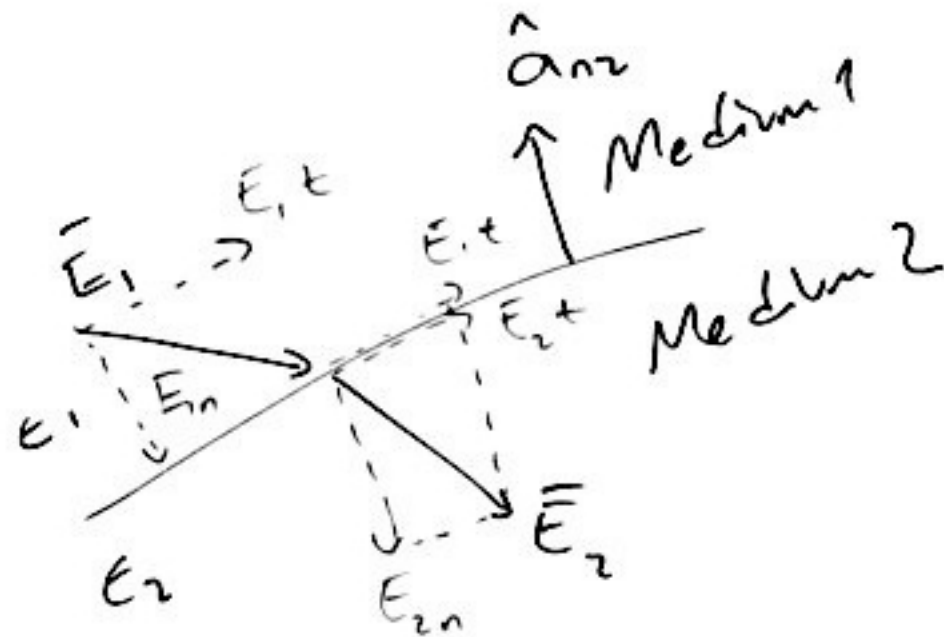


Boundary Conditions for Electrostatics:



1.) $E_{1t} = E_{2t}$

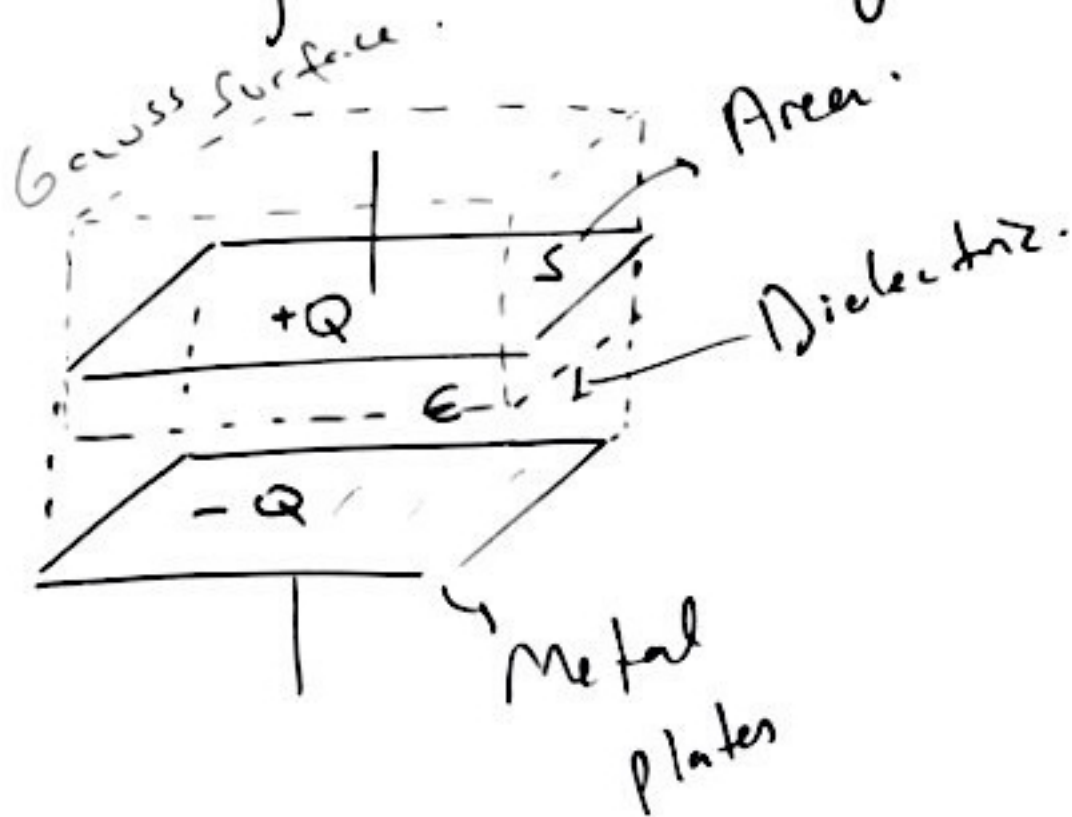
Tangential components of \vec{E} are continuous across the interface.

$\hat{a}_{nz} \cdot (\vec{D}_1 - \vec{D}_2) = \rho_s$ ($\frac{C}{m^2}$) surface

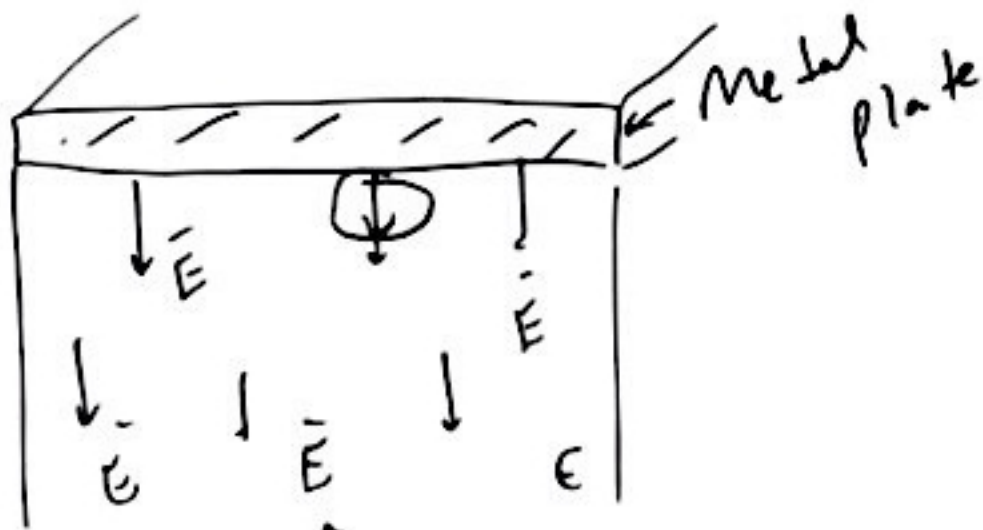
2.) $D_{1n} - D_{2n} = \rho_s$ Free charge density

Ex:

Find the \vec{E} -field in a parallel plate capacitor using the boundary condition.



Ans:

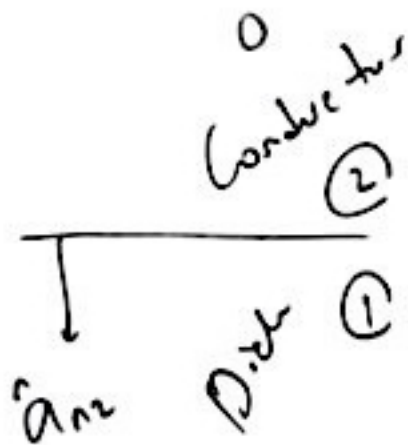


Assume that \vec{E} is uniform and constant everywhere.
(we neglect the fringe field)

This assumption enables us to evaluate the \vec{E} -field everywhere by evaluating it at the boundary.

$$D_{1n} - D_{2n} = (\rho_s) \rightarrow \rho_s = \frac{Q}{S}$$

$$\epsilon_1 E_1 - \epsilon_2 E_2 = \frac{Q}{S}$$



$$\epsilon_1 E_1 = \frac{Q}{S}$$

or

$$\boxed{E_1 = \frac{Q}{\epsilon_1 S}} \left(\frac{V}{m} \right)$$

2. Method (Gauss law):

$$\oint \vec{D} \cdot \vec{d}\vec{s} = Q$$

$$\epsilon E \cdot S = Q$$

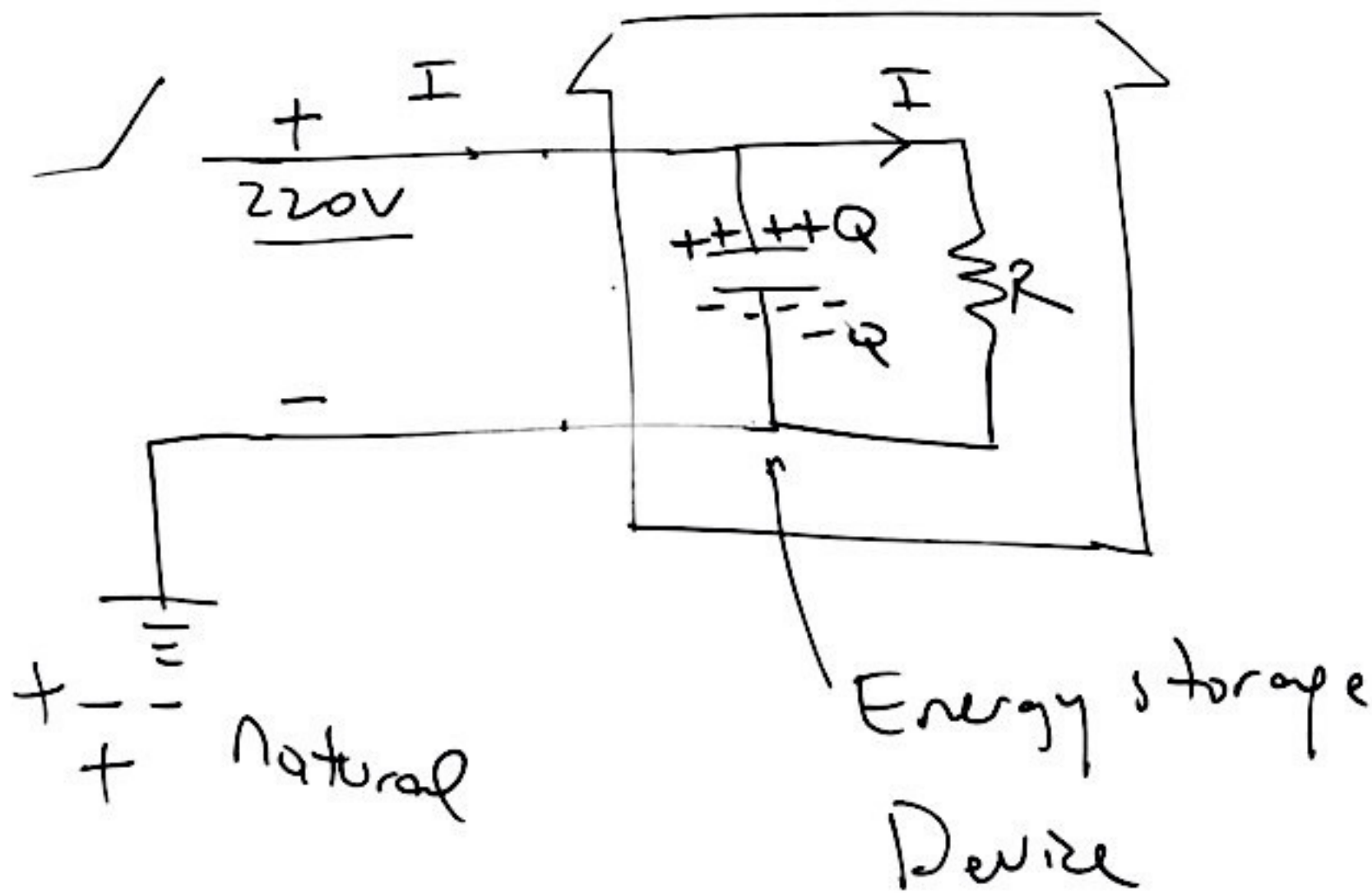
$$\boxed{E = \frac{Q}{\epsilon S}}$$

Capacitance and Capacitors:

$$C = \frac{Q}{V} \quad \left(\frac{\text{Coulombs}}{\text{Volt}} = \text{Farad} \right)$$

Charge

Voltage



Measure of that Energy Storage:

Capacitance = C .

$$C = \frac{Q}{V}$$

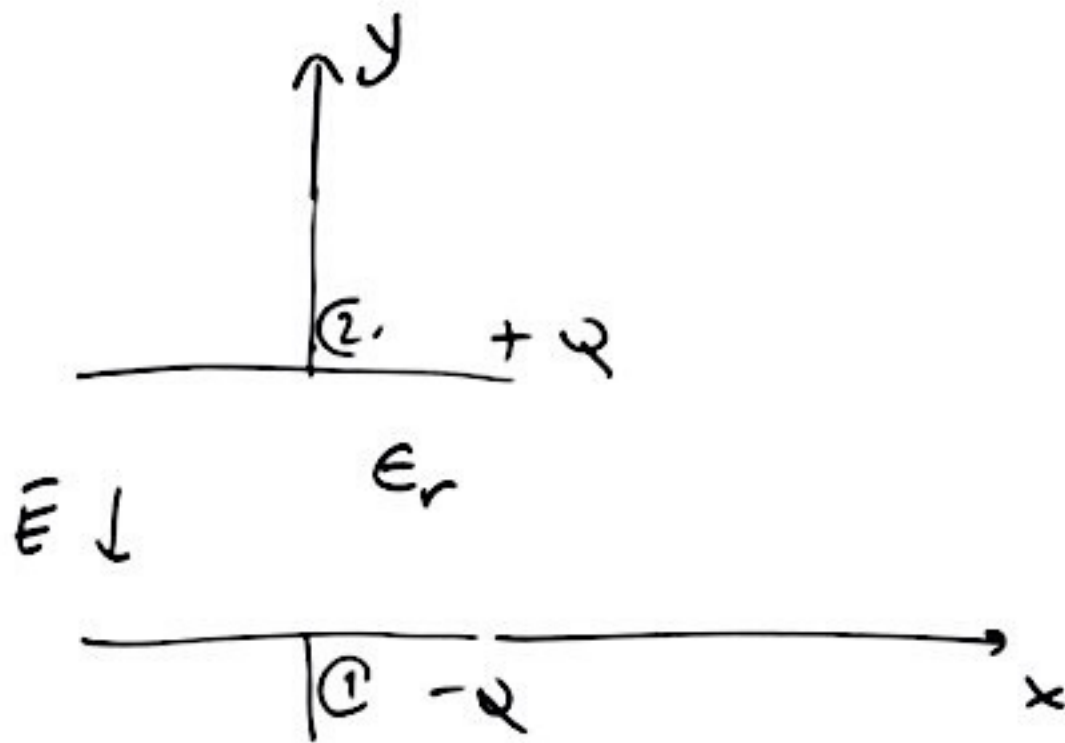
(Per volt, how much charge it can store is the capacitance.)

Capacitor is the name for an electrical device with capacitance.

Ex:

Determine the capacitance of a parallel plate capacitor.

Ans:



$$\vec{E} = -\hat{a}_y \frac{Q}{\epsilon S} \quad (\text{as before})$$

$$\begin{aligned} V_{12} &= - \int_{l_1}^{l_2} \vec{E} \cdot d\vec{l} = - \int_0^d \left(-\hat{a}_y \frac{Q}{\epsilon S} \right) \cdot (\hat{a}_y dy) \\ &= \int_0^d \frac{Q}{\epsilon S} dy = \frac{Q d}{\epsilon S} \quad (v) \end{aligned}$$

Then,

$$C = \frac{Q}{V} = \epsilon \frac{S}{d} \quad (f)$$

Steps to find Capacitance:

1-1 Choose an appropriate coord. system for the given problem.

2-1 Assume $+Q$ and $-Q$ charges on the conductors.

3-1 Find \vec{E}

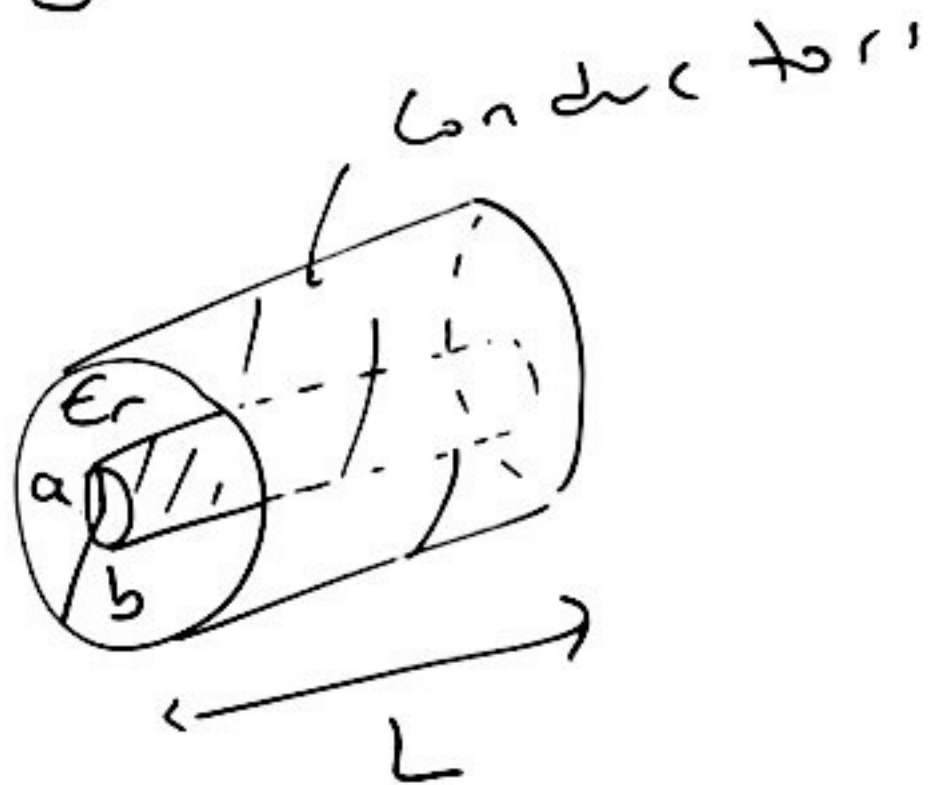
4-1 Find V from $V = - \int_{P_1}^{P_2} \vec{E} \cdot d\vec{l}$.

5-1 Find C from

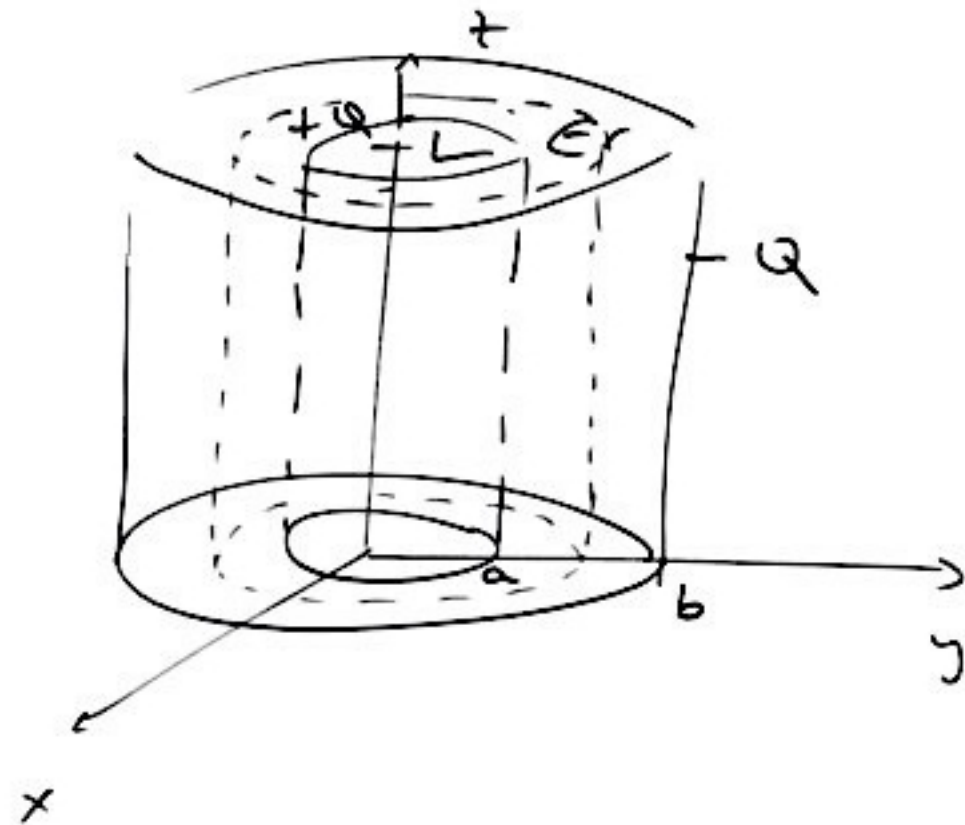
$$C = \frac{Q}{V}$$

Ex:

Find the capacitance of a coaxial cable of length L , filled with dielectric of ϵ_r . Given as



Ans:



The Electric field inside the dielectric π :

$$\vec{E}_r = \hat{a}_r E_r$$

$$E_r = \frac{Q}{2\pi \epsilon L r} \left(\frac{V}{\ln} \right)$$

$$V = - \int_{r=b}^{r=a} \vec{E} \cdot d\vec{u} = - \int_b^a \left(\hat{a}_r \frac{Q}{2\pi \epsilon L r} \right) \cdot (\hat{a}_r dr)$$

or

$$V = \frac{Q}{2\pi\epsilon L} \int_b^a \frac{1}{r} dr$$

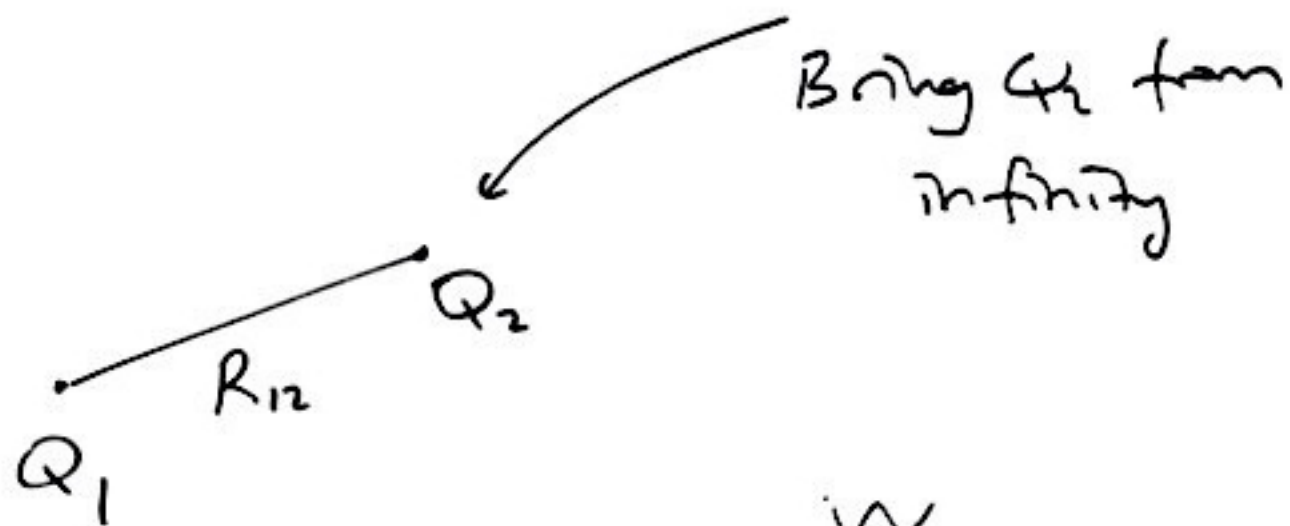
or

$$V = \frac{Q}{2\pi\epsilon L} \ln\left(\frac{b}{a}\right)$$

Then,

$$C = \frac{Q}{V} = \frac{2\pi\epsilon L}{\ln\left(\frac{b}{a}\right)} \quad (F)$$

Electrostatic Energy:



$$\text{Work} = W_2 = Q_2 \underbrace{V_2}_{\frac{W}{Q}}$$

By definition, the voltage at a single point such as V_2 is defined as

$$V_2 = - \int_{\infty}^R \vec{E} \cdot \vec{dl} = - \int_{\infty}^R \left(\hat{a}_r \frac{Q}{4\pi\epsilon_0 R^2} \right) \cdot (\hat{a}_r dR)$$
$$= \frac{Q}{4\pi\epsilon_0 R} \text{ (V)}$$

$$V_{12} = \underbrace{V_2}_{P_2} - \underbrace{V_1}_{P_1} = - \int_{P_1}^{P_2} \vec{E} \cdot \vec{dl}$$

$$W_2 = Q_2 \frac{Q_1}{4\pi\epsilon_0 R_{12}} = Q_1 \frac{Q_2}{4\pi\epsilon_0 R_{12}} = Q_1 V_1$$

or

$$W_2 = \frac{1}{2} (Q_1 V_1 + Q_2 V_2)$$

If we bring another charge Q_3 from infinity.
:

$$W_3 = \frac{1}{2} (Q_1 V_1 + Q_2 V_2 + Q_3 V_3)$$

:

$$W_e = \frac{1}{2} \sum_{k=1}^N Q_k V_k \quad \text{for } N \text{ charges}$$

This is the potential energy stored in the system.

• Q_2

• Q_1 • Q_3 • Q_4

If the charge distribution is continuous:



$$W_e = \frac{1}{2} \int_{V'} \rho V d\tau \quad (3)$$

In this equation

$$W_e = \frac{1}{2} \int_{V'} (\bar{\nabla} \cdot \bar{D}) V d\tau$$

Using the identity

$$\bar{\nabla} \cdot (V \bar{D}) = V \bar{\nabla} \cdot \bar{D} + \bar{D} \cdot \bar{\nabla} V$$

$$W_e = \frac{1}{2} \int_{V'} \bar{\nabla} \cdot (V \bar{D}) d\tau - \frac{1}{2} \int_{V'} \bar{D} \cdot \bar{\nabla} V d\tau$$

$$= \frac{1}{2} \oint_{S'} V \bar{D} \cdot \hat{a}_n ds + \frac{1}{2} \int_{V'} \bar{D} \cdot \bar{E} d\tau$$

○

Because:

$$\text{As } R \rightarrow \infty$$

$$V \propto \frac{1}{R}$$

$$D \propto \frac{1}{R^2}$$

Thus,

$$W_e = \frac{1}{2} \int_{v'} \bar{D} \cdot \bar{E} \, dv$$

or

$$W_e = \frac{1}{2} \int_{v'} \epsilon E^2 \, dv$$

or

$$W_e = \frac{1}{2} \int_{v'} \frac{D^2}{\epsilon} \, dv$$

Hence

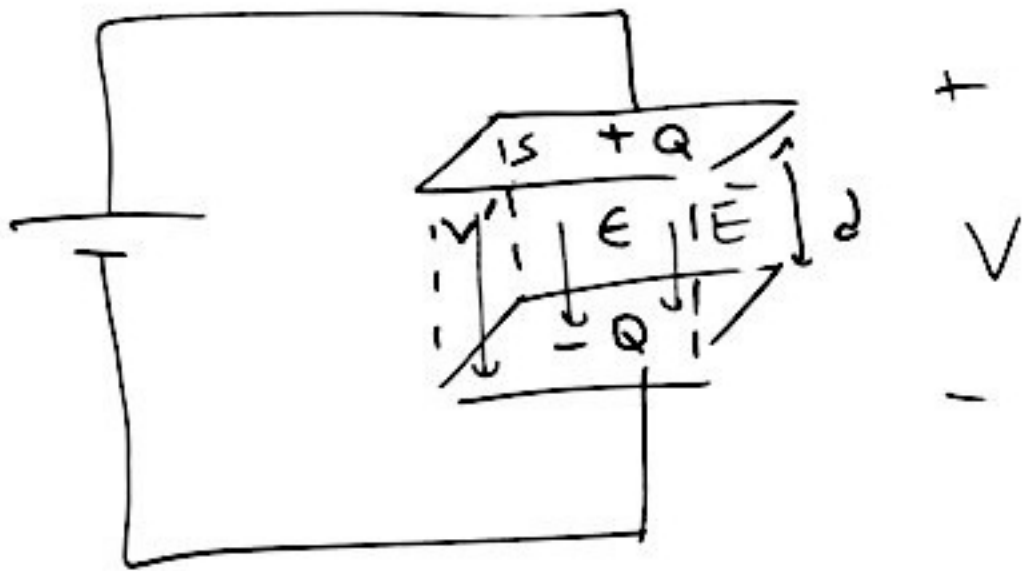
$$w_e = \text{energy density} = \frac{1}{2} \epsilon E^2 \quad \left(\frac{J}{m^3} \right)$$

Ex:

Parallel plate capacitor of area S and separation d is charged to a voltage V .

The permittivity of the dielectric is ϵ .

Find the stored energy
electrostatic



Ans:

$$E = \frac{V}{d}$$

$$W_e = \frac{1}{2} \int_{v'} \epsilon \left(\frac{v}{d} \right)^2 dv' = \frac{1}{2} \epsilon \left(\frac{v}{d} \right)^2 (Sd)$$

$$= \frac{1}{2} \underbrace{\left(\epsilon \frac{S}{d} \right)}_C v^2$$

$$W_e = \frac{1}{2} C v^2 \quad (3)$$

Since $Q = C v$

$$W_e = \frac{1}{2} Q v \quad (3)$$

or

$$W_e = \frac{Q^2}{2C} \quad (3)$$

Chp. 5. Steady Electric Currents:

$$I = \frac{Q}{t} \quad \left(\frac{C}{\text{sec}} = \text{Ampere} \right)$$

The current density \vec{J} is defined as

$$\vec{J} = \rho \vec{v} \quad \left(\frac{A}{m^2} \right)$$

where

$$\rho = \text{Charge density} \quad \left(\frac{C}{m^3} \right)$$

and

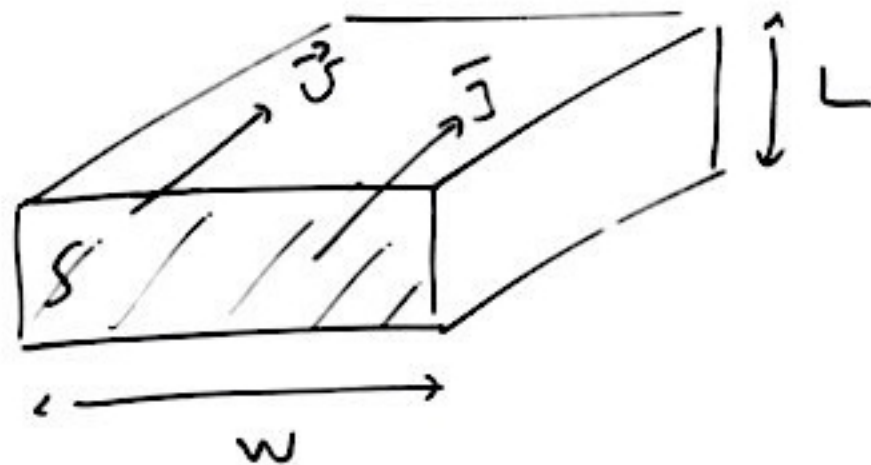
$$\vec{v} = \text{Charge velocity} \quad \left(\frac{m}{\text{sec}} \right)$$

The current density \vec{J} is related to the current I as

$$I = \int_S \vec{J} \cdot d\vec{s}$$

Ex:

In the given figure calculate the current in terms of the current density \vec{J} .

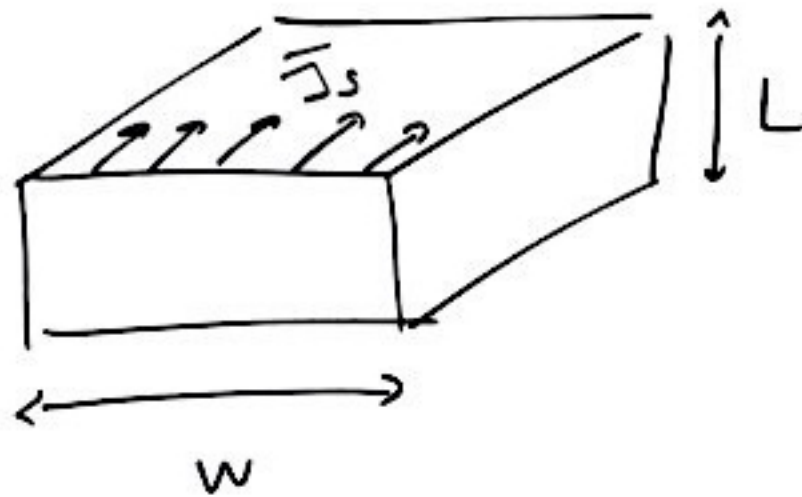


Assuming \vec{J} is steady and uniform
not changing with time The same everywhere.

Ans:

$$I = \int \vec{J} \cdot \hat{j}_1 = w \cdot L \cdot J \text{ (A)}$$

Surface Current density \vec{J}_s ($\frac{A}{m}$)



Assume \vec{J}_s Uniform \vec{J}_s on the top surface.

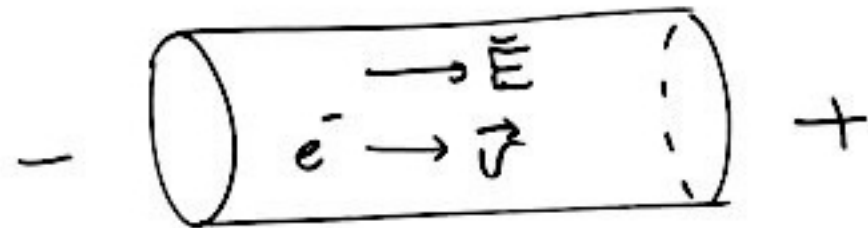
$$I = \int_C \vec{J}_s \cdot d\vec{\ell}$$

$$I = L \cdot J_s \text{ (A)}$$

For most conducting materials,

$$\vec{v} = -\mu_e \vec{E}$$

where $\mu_e =$ Mobility of electrons. ($\text{m}^2/\text{V}\cdot\text{s}$)



We have

$$\vec{J} = q \vec{v} = -q \mu_e \vec{E}$$

or

$$\vec{J} = \sigma \vec{E} \quad \left(\frac{\text{A}}{\text{m}^2} \right)$$

where

$$\sigma = \text{Conductivity} \quad \left(\frac{\text{S}}{\text{m}} \right)$$

$$\sigma_{\text{Copper}} = 5.8 \times 10^7 \left(\frac{\text{S}}{\text{m}}\right)$$

Conductor

$$\sigma_{\text{Germanium}} = 2.2 \left(\frac{\text{S}}{\text{m}}\right)$$

$$\sigma_{\text{Silicon}} = 1.6 \times 10^{-3} \left(\frac{\text{S}}{\text{m}}\right)$$

$$\sigma_{\text{Rubber}} = 10^{-11} \left(\frac{\text{S}}{\text{m}}\right)$$

} Semi-Conductor

} Insulator

Define

$$\frac{1}{\sigma} = \rho = \text{Resistivity } (\Omega \cdot \text{m})$$

Ex:

Find the Resistance of a conductor



Uniform field distributions are assumed.

Then,

$$V = E \cdot l$$

or

$$E = \frac{V}{l}$$

and

$$\bar{I} = \int \bar{j} \cdot \bar{ds} = jS$$

or

$$j = \frac{I}{S}$$

Now, we have

$$\bar{j} = \sigma \bar{E}$$

or

$$j = \sigma E$$

or

$$\frac{I}{S} = \sigma \frac{V}{l}$$

or

$$V = \underbrace{\left(\frac{l}{\sigma S}\right)}_R I \quad (\text{Ohm's law in volumetric form})$$

Then,

$$R = \frac{l}{\sigma S} \quad (\Omega)$$

Power Dissipation:

$$p = \lim_{\Delta t \rightarrow 0} \frac{\Delta w}{\Delta t} = q \vec{E} \cdot \vec{v}$$

$\nearrow \frac{F}{q} \quad \nearrow \frac{\Delta x}{\Delta t}$

(power correspond to moving a charge q against an electric field \vec{E})

The power delivered to all charges in volume dv is

$$dP = \sum p = E \cdot \left(\sum q \vec{v}\right) dv$$

$$\text{or } dP = \vec{E} \cdot \vec{J} dv$$

(Integrating both sides in volume

V

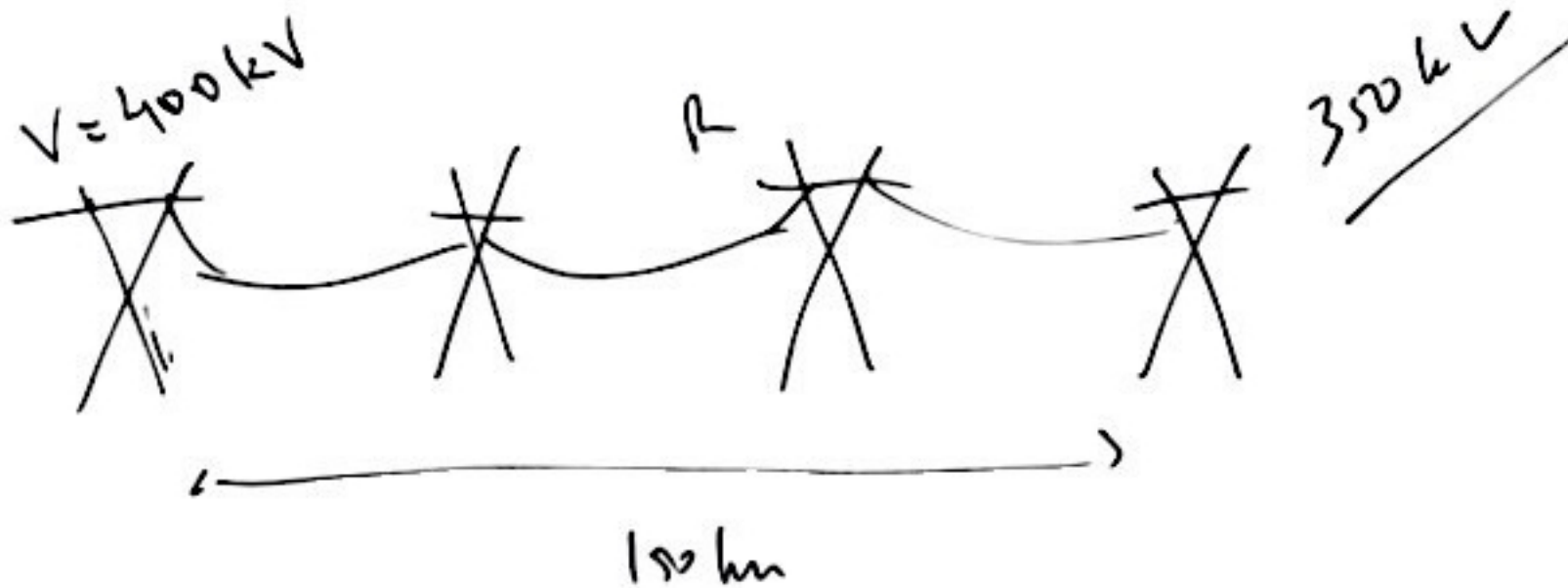
$$P = \int_V \vec{E} \cdot \vec{J} \, dv \quad (\text{w})$$

$$= \int_L \epsilon \vec{E} \int_S \vec{J} \cdot \vec{dS} = V \cdot I \quad (\text{w})$$

(IR)

or

$$P = I^2 R \quad (\text{w})$$



Equation of Continuity:

This equation gives the relation between the current density and charge.

$$\vec{\nabla} \cdot \vec{J} = -\frac{\partial \rho}{\partial t}$$

For steady currents

$$\frac{\partial}{\partial t} = 0$$

Then,

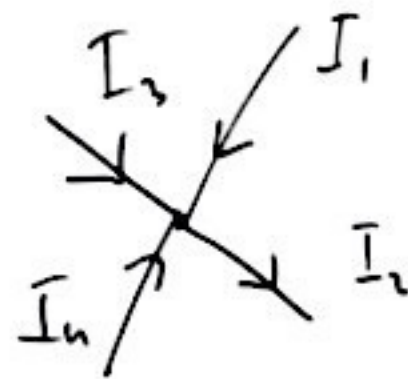
$$\vec{\nabla} \cdot \vec{J} = 0$$

Take the

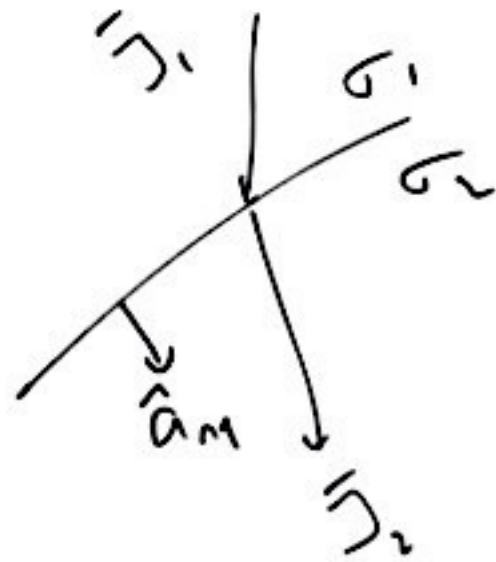
integral of both sides

$$\int_V \vec{\nabla} \cdot \vec{J} = 0$$

$$\text{or } \sum_j I_j = 0 \text{ (A)} \quad (\text{Kirchoff's current law})$$



Boundary Conditions for Current
Density:



$$J_{1n} = J_{2n}$$

$$\frac{J_{1t}}{J_{2t}} = \frac{\sigma_1}{\sigma_2}$$

Resistance Calculations:

Steps:

- 1-) Choose the coord. system.
- 2-) Assume a potential difference V_0 between conductor terminals.
- 3-) Find \vec{E} within the conductor.
- 4-) Find the total current

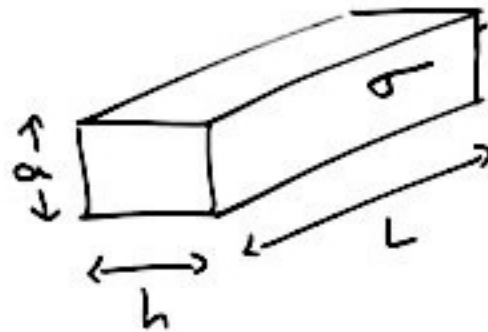
$$I = \int \vec{j} \cdot d\vec{s} = \int \sigma \vec{E} \cdot d\vec{s}$$

- 5-) Find the resistance

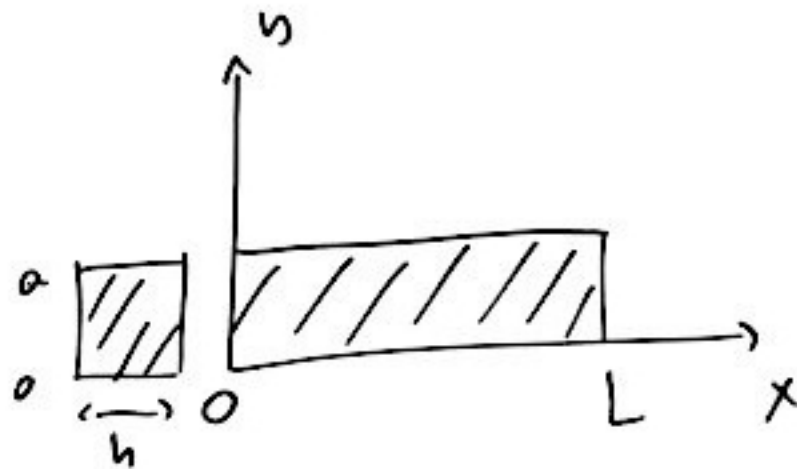
from $R = \frac{V_0}{I}$.

Ex:

Find the resistance of the material



Ans:



$$V=0 \text{ at } x=0$$

$$V=V_0 \text{ at } x=L$$

$E = E(x)$ only.

In order to find E :

or $\bar{\nabla} \cdot \bar{D} = \rho$

or $\bar{\nabla} \cdot \epsilon \bar{E} = \rho$

or

$$\bar{\nabla} \cdot (\epsilon \bar{\nabla} V) = -\rho$$

$$\nabla \cdot (\bar{\nabla} V) = -\frac{\rho}{\epsilon}$$

or

$$\boxed{\nabla^2 V = -\frac{\rho}{\epsilon}} \quad (\text{Poisson's equation})$$

∇^2 is called the Laplacian operator

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} \quad (\text{in cartesian word.})$$

Since we want to find the solution of the \vec{E} -field within the conducting material, we assume the free charge density $\rho = 0$ inside the material.

Thus, we need to solve

$$\nabla^2 V = 0 \quad (\text{Laplace equation})$$

with boundary conditions

$$\begin{array}{l} V = 0 \text{ at } x = 0 \\ \text{and} \\ V = V_0 \text{ at } x = L \end{array}$$

$\nabla^2 V = 0$ gives

$$\frac{\partial^2 V}{\partial x^2} = 0$$

The general solution is

$$V(x) = C_1 x + C_2$$

Where C_1 and C_2 are constants to be determined by the boundary conditions.

$$C_2 = 0, \quad C_1 = \frac{U_0}{L}$$

$$V(x) = \frac{U_0}{L} x$$

$$\bar{E} = -\bar{\nabla} V = -\hat{a}_x \frac{U_0}{L}$$

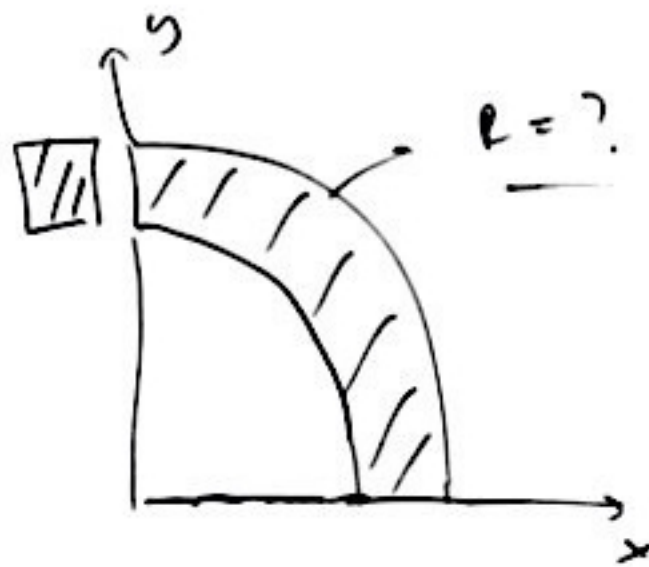
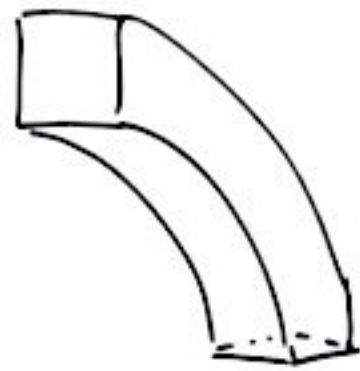
$$\bar{J} = \sigma \bar{E} = -\sigma \bar{\nabla} V = -\hat{a}_x \frac{\sigma U_0}{L}$$

$$I = \int_S \bar{J} \cdot \bar{d}s = \int_S \left(-\hat{a}_x \frac{\sigma U_0}{L} \right) \cdot \left(-\hat{a}_y dy dz \right)$$

$$= \frac{\sigma U_0}{L} (ah)$$

$$, \quad R = \frac{U_0}{I} = \frac{U_0}{\frac{\sigma U_0}{L} (ah)} = \frac{L}{\sigma (ah)} \quad (\Omega)$$

Ex: 5.6 PS 218



Q. 6. Static Magnetic Fields:

$$\frac{\partial}{\partial t} = 0$$



$$q_t \quad \vec{F}_m$$

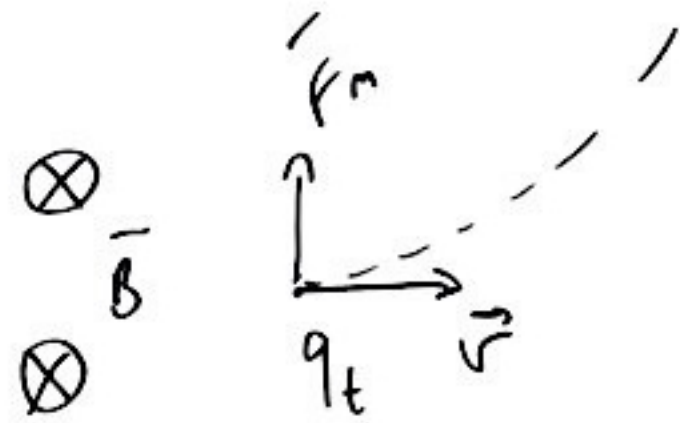
\vec{B} = Magnetic Field $\left(\frac{Wb}{m^2}\right)$

Density Vector

$$\vec{E} \rightarrow \vec{F}_e = \vec{E} \cdot q_t$$

$$\vec{F}_m = q_t \vec{v} \times \vec{B}$$

velocity vector.



$$\int \vec{E} \cdot d\vec{l} = \frac{Q}{\epsilon}$$

$$\vec{E} = \int \frac{1}{r^2} \hat{r} dq'$$

$$\begin{aligned} \vec{F}_{total} &= \vec{F}_e + \vec{F}_m \\ &= \vec{E} q + q \vec{v} \times \vec{B} \\ &= q (\vec{E} + \vec{v} \times \vec{B}) \quad (\text{Lorentz equation}) \end{aligned}$$

$$\frac{1 \text{ Wb}}{\text{m}^2} = 1 \text{ Tesla} = 10^4 \text{ Gauss}$$

Postulates for Magnetostatics.

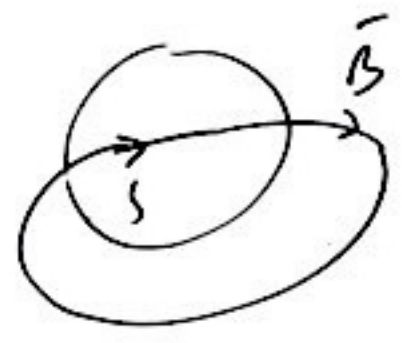
$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

Integral forms are

$$\oint_S \vec{B} \cdot d\vec{s} = 0$$

Magn. field lines always close upon themselves.



Stokes' theorem

$$\int_S (\vec{\nabla} \times \vec{B}) \cdot d\vec{s} = \mu_0 \int_S \vec{J} \cdot d\vec{s}$$

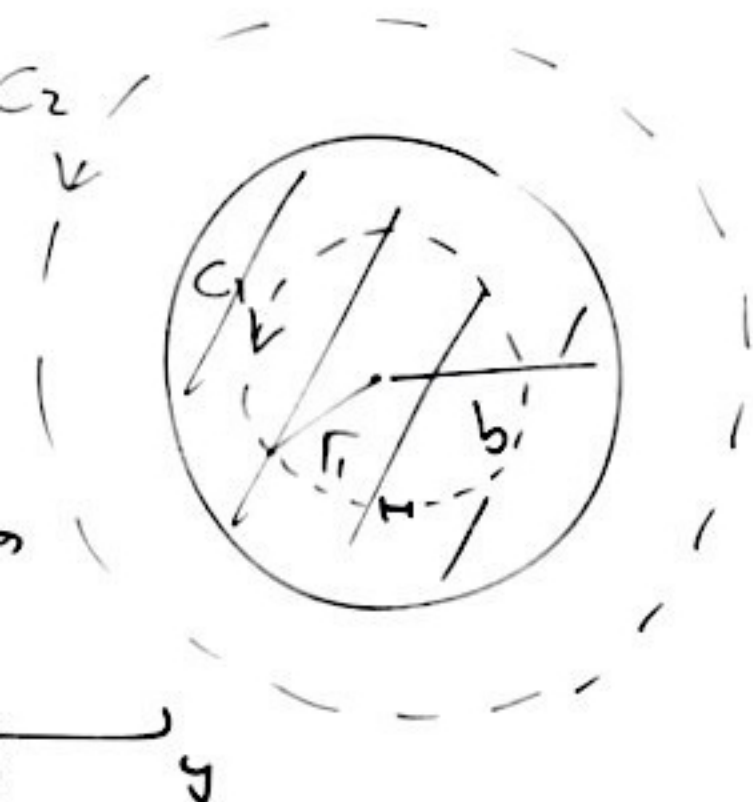
$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 I$$

(Ampere's law)

Ex: 6.1

An infinitely long, straight conductor with a circular cross section of radius b carries a steady current I . Determine the magnetic flux density both inside and outside the conductor.

Ans:



Inside the Conductor:

$$\vec{B}_1 = \hat{a}_\phi B_{\phi 1}$$

$$\oint_{C_1} \vec{B}_1 \cdot d\vec{L} = \mu_0 \left(\frac{I}{2} \right)$$

The current passing through the contour C_1 .

$$\int_0^{2\pi} (\hat{a}_\phi B_{\phi 1}) \cdot (r_1 d\phi) = \mu_0 \left(\frac{r_1^2}{b^2} \right) I$$

The current inside the circle

$$\vec{B}_1 = \hat{a}_\phi B_{\phi 1} = \hat{a}_\phi \frac{\mu_0 r_1 I}{2\pi b^2} \quad r_1 \leq b$$

Outside the conductor:

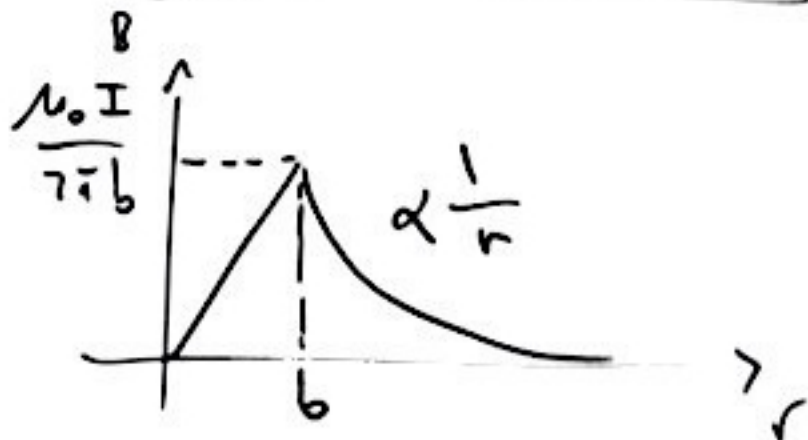
$$\vec{B}_2 = \hat{a}_\phi B_{\phi 2} \quad \vec{\ell} = \hat{a}_\phi r_2 \Delta\phi$$

$$\oint_{C_2} \vec{B}_2 \cdot \vec{\ell} = 2\pi r_2 B_{\phi 2}$$

$$2\pi r_2 B_{\phi 2} = \mu_0 I$$

Thus,

$$B_{\phi 2} = \frac{\mu_0 I}{2\pi r_2} \left(\frac{\text{wb}}{\text{m}^2} \right) \quad r_2 \geq b$$



Magnetic Field!

This is also a force field.

$$\vec{F}_m = q \vec{v} \times \vec{B}$$

↳ Magnetic flux density vector ($\frac{Wb}{m^2}$)

Two equations for static magnetic field:

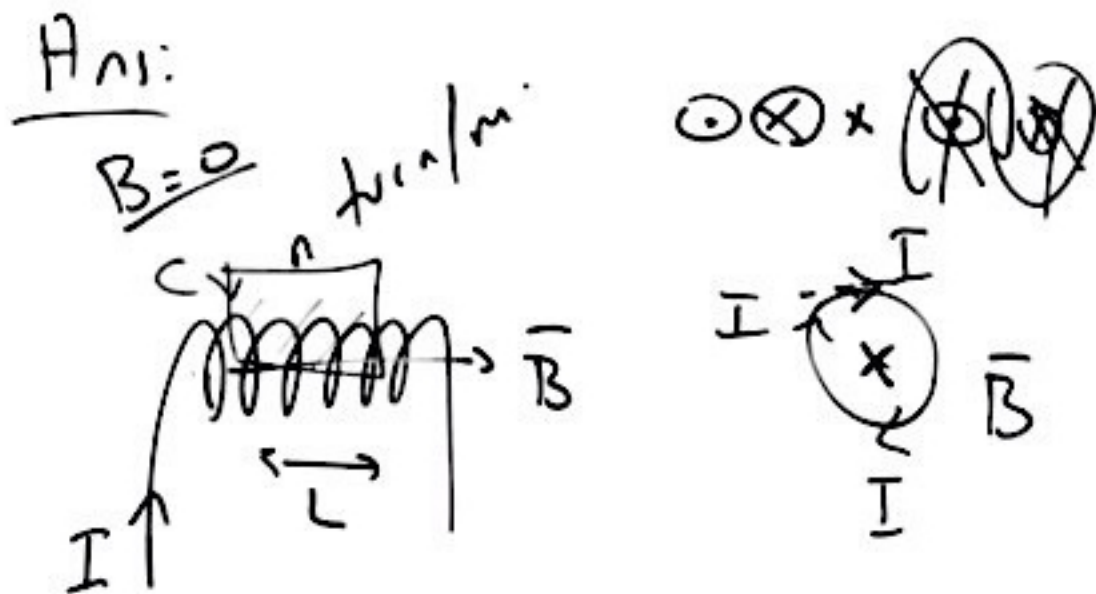
$$\vec{\nabla} \cdot \vec{B} = 0 \quad \rightarrow \quad \oint_S \vec{B} \cdot d\vec{s} = 0$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J} \quad \rightarrow \quad \oint_C \vec{B} \cdot d\vec{l} = \mu_0 I \quad (\text{Ampere's law})$$

Ex:

Determine the magnetic field density vector \vec{B} inside an infinitely long solenoid with air core having n turns per unit length and carrying a current I .

Ans:



$$\oint_C \vec{B} \cdot d\vec{l} = \int_0^L (\hat{a}_x B_x) \cdot (\hat{a}_x dx) = \mu_0 n L I$$

$$B_x \int_0^L dx = \mu_0 n L I \Rightarrow \boxed{B_x = \mu_0 n I \frac{Wb}{m}}$$

If

$$\mu_0 = 4\pi \times 10^{-7}$$

$$I = 10 \text{ A}$$

$$n = ?$$

$$B = 20,000 \text{ Gauss}$$

$$\left(1 \frac{\text{Wb}}{\text{m}^2} = 10^4 \text{ Gauss} \right)$$

$$\Rightarrow 20,000 \text{ Gauss} = 2 \frac{\text{Wb}}{\text{m}^2}$$

Thus

$$n = \frac{\mu_0}{4\pi \times 10^{-7} \times 10} = \frac{1}{6} \times 10^6$$

$$\approx 0.17 \times 10^6$$

$$\approx 170 \times 10^3$$

$$\approx 170,000 \text{ turns per unit length}$$

$$\sigma = \frac{1}{\rho} = \delta$$

$$\vec{J} = \sigma \vec{E}$$

$$\text{Power loss} = \int_V \vec{E} \cdot \vec{J} \cdot dV = \int_V \sigma |\vec{E}|^2 dV = I^2 R \text{ (W)}$$

170,000 turns per meter is very difficult.

Vector Magnetic Potential:

It's defined by

$$\vec{B} = \nabla \times \vec{A}$$

where

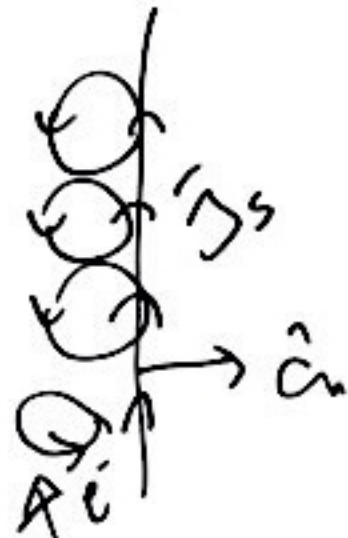
\vec{A} = Vector magnetic potential

This concept is similar to electric potential (V).

In integral evaluations of the electric field, the voltage (V) is easier to find since it depends upon $\frac{1}{r}$ and the electric field $\propto \frac{1}{r^2}$.

In calculating the magnetic field, it's also easier to use the vector potential \vec{A} than \vec{B} .

Magnetization



If magnetized



\vec{m} = magnetic dipole moment.
 $= \hat{n} I S$

$$\vec{M} = \frac{\sum \vec{m}}{dV} \quad (\text{Magnetization vector})$$

$$\vec{J}_m = \nabla \times \vec{M}$$
$$\vec{J}_s = \vec{M} \times \hat{n}$$

$$\frac{1}{\mu_0} \nabla \times \vec{B} = \vec{J} + \vec{J}_m = \vec{J} + \nabla \times \vec{M}$$

$$\nabla \times \left(\frac{\vec{B}}{\mu_0} - \vec{M} \right) = \vec{J}$$

$\vec{H} = \text{Mag. field}$

Intensity vector.

$$\nabla \times \vec{H} = \vec{J}$$



$$\oint_C \vec{H} \cdot d\vec{l} = I$$

(Ampere's law general form)

$$\vec{M} = \chi_m \vec{H}$$

↳ magnetic susceptibility

$$\vec{B} = \mu_0 (1 + \chi_m) \vec{H}$$

$$= \mu_0 \mu_r \vec{H} = \mu \vec{H}$$

↳ permeability

$$\vec{B} = \mu \vec{H}$$

$$\vec{H} = \frac{\vec{B}}{\mu}$$

Diamagnetic Materials:

$$\mu_r \lesssim 1$$

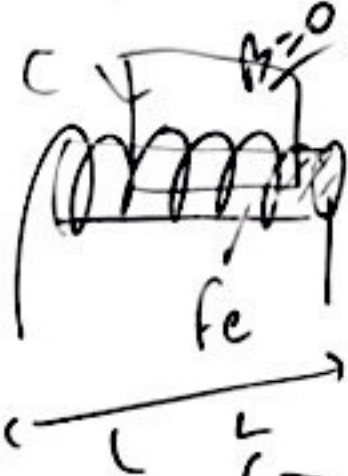
Paramagnetic: $\mu_r \gtrsim 1$

Ferromagnetic: $\mu_r \gg 1$

↳ Ferrites:

Ex:

Fe (iron) $\mu_r = 7000$.



Solenoid

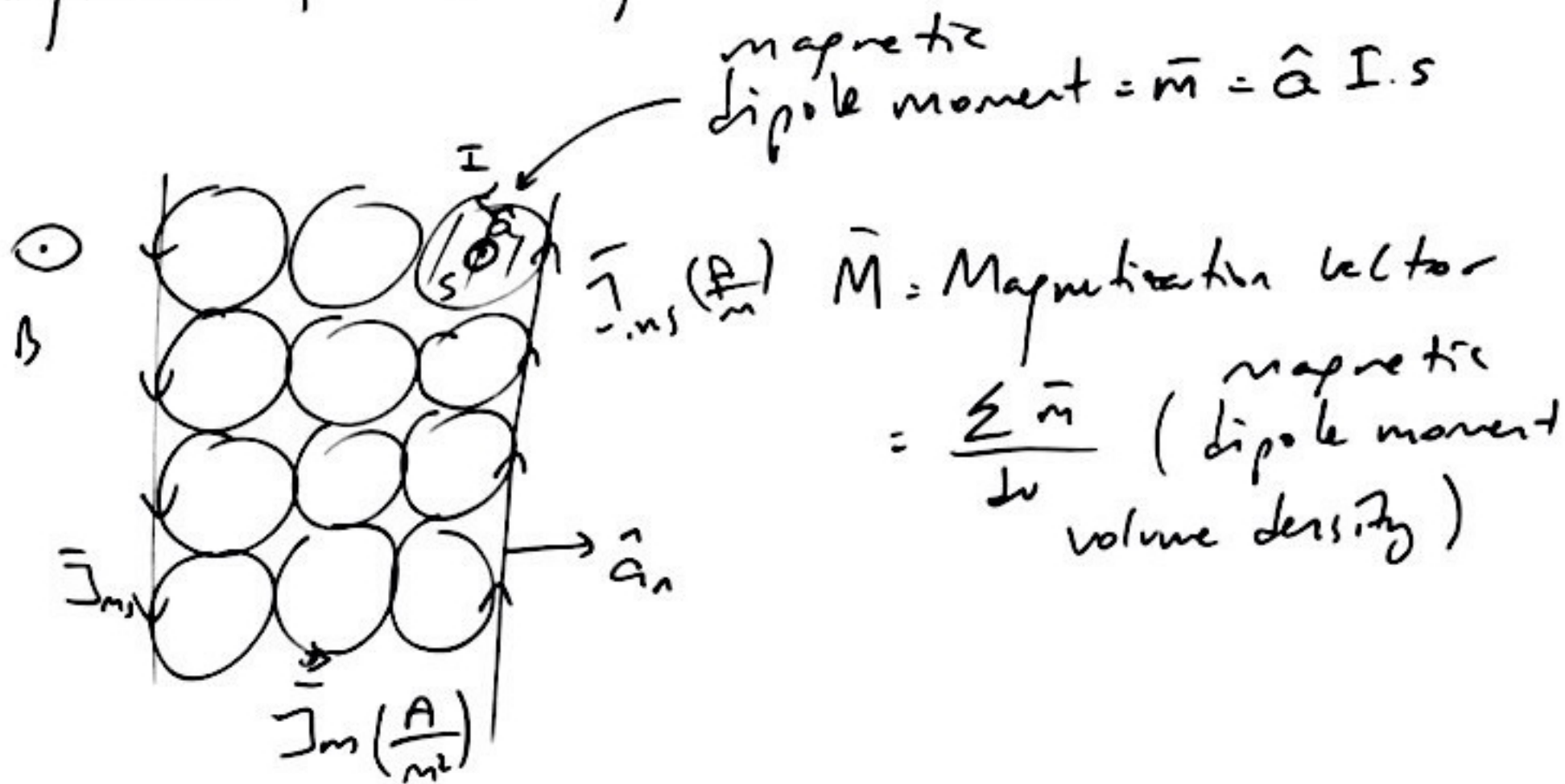
$$\int \vec{H} \cdot d\vec{l} = nLI$$

0

$$= \frac{B \cdot L}{\mu_r \mu_0} = nLI = \mu_r \mu_0 n^2 I^2 L \left(\frac{W}{m^2} \right)$$

Magnetization:

When magnetized materials are put inside a magnetic field, magnetization occurs.



$$\vec{J}_m = \vec{\nabla} \times \vec{M}$$

$$\vec{J}_m = \vec{M} \times \vec{a}_n$$

$$\frac{1}{\mu_0} \nabla \times \vec{B} = \vec{J} + \vec{J}_m = \vec{J} + \nabla \times \vec{M}$$

$$\nabla \times \left(\underbrace{\frac{\vec{B}}{\mu_0} - \vec{M}}_{\vec{H}} \right) = \vec{J}$$

$$\int_S \nabla \times \vec{H} \cdot d\vec{s} = \int_S \vec{J} \cdot d\vec{s}$$

$$\oint_C \vec{H} \cdot d\vec{l} = I \quad (\text{Ampere's law})$$

and

$$\vec{M} = \chi_m \vec{H}$$

→ Magnetic susceptibility

$$\begin{aligned}\vec{B} &= \mu_0 (1 + \chi_m) \vec{H} \\ &= \mu_0 \mu_r \vec{H} = \mu \vec{H} \quad \left(\frac{\text{wb}}{\text{m}^2} \right)\end{aligned}$$

or

$$\vec{H} = \frac{1}{\mu} \vec{B}$$

where

μ = magnetic permeability.

μ_r = Relative permeability.

Materials:

Diamagnetic, $\mu_r \leq 1$

Paramagnetic, $\mu_r \approx 1$

Ferromagnetic, $\mu_r \gg 1$ (Fe)

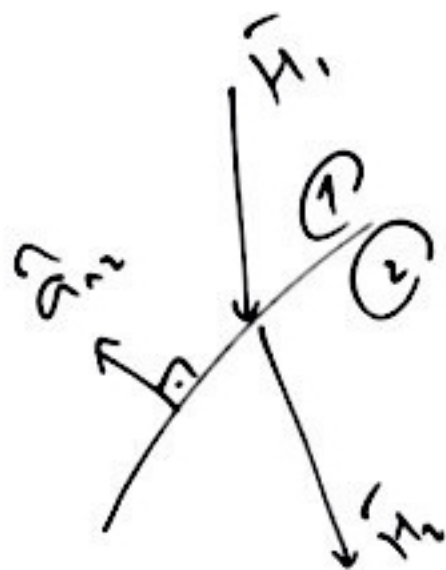
$\hookrightarrow \mu_r = 7000$

Boundary Conditions for Static
Magnetic Field:

$B_{1n} = B_{2n}$ or for magnetized media

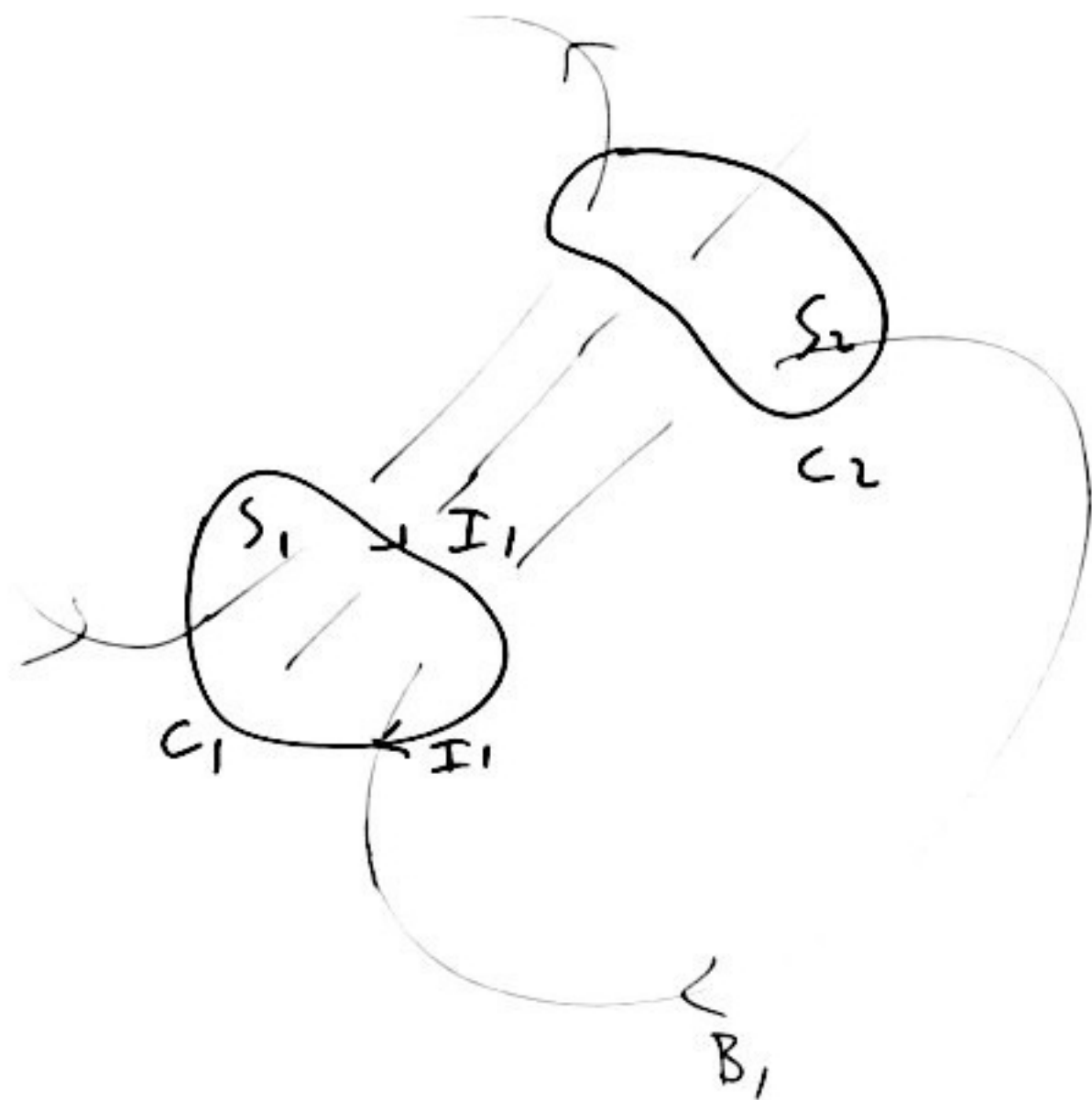
$$\mu_1 H_{1n} = \mu_2 H_{2n} \quad (\text{Normal component})$$

and



$$\hat{a}_{n2} \times (\bar{H}_1 - \bar{H}_2) = \bar{J}_s \quad (\text{Tangential component})$$

Inductances and Inductors:



Define

$$\phi_{12} = \int_{S_2} \vec{B}_1 \cdot d\vec{S}_2 \quad (\text{wb}) \quad (\text{Flux on } S_2 \text{ created by } \vec{B}_1 \text{ on } S_1 \text{ or } C_1)$$

Since $B \propto I_1$,

$$\phi_{12} \propto I_1$$

and

$$\phi_{12} = L_{12} I_1$$

where

L_{12} = Mutual inductance. (Henry)

In case C_2 has N_2 turns,

$$\Lambda_{12} = N_2 \phi_{12} \text{ (wb)}$$

Then

$$\Lambda_{12} = L_{12} I_1$$

or

$$L_{12} = \frac{\Lambda_{12}}{I_1} \text{ (H)}$$

(More general formula for mutual inductance.)

Self Inductance

Flux linkage per unit current in the loop C_1 itself.

$$L_{11} = \frac{\Lambda_{11}}{I_1}$$

or

In general,

$$L = \frac{\Lambda}{I} \text{ (H)}$$

Steps to find Inductance (Self inductance)

- 1-) Choose an appropriate coord. system.
- 2-) Assume a current I in the conducting wire.
- 3-) Find \vec{B}
- 4-) Find $\phi = \int \vec{B} \cdot d\vec{s}$

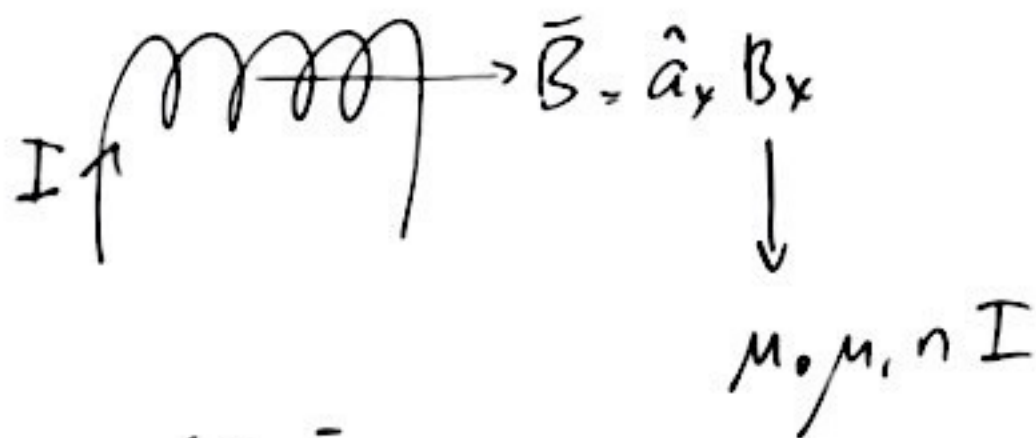
5.) Find $\Lambda = N\Phi$

(.) Find $L = \frac{\Lambda}{I}$.

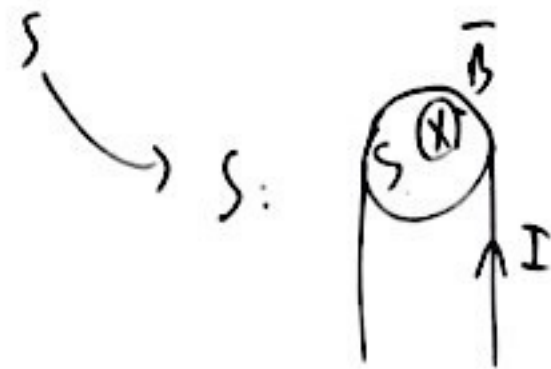
Ex.

Find the inductance of a solenoid
with iron core ($\mu_r = 7000$)
having n turns.

Ans:



$$\phi = \int \vec{B} \cdot \vec{d}s$$



$$\begin{aligned} \phi &= \int_0^{2\pi} \int_0^r \vec{B} \cdot \vec{d}s \\ &= (\pi r^2) \cdot B_x = S B_x \text{ (wb)} \\ &= S \mu_0 \mu_r n I \end{aligned}$$

$$\Lambda = n \phi = S \mu_0 \mu_r n^2 I \text{ (wb)}$$

$$L = \frac{\Lambda}{I} = S \mu_0 \mu_r n^2 \text{ (H)}$$

Note that the number of turns (n) is an important parameter to adjust the inductance ($L \propto n^2$)

In order to find the magnetic field due to current carrying conductors, we have been using the Ampere's law, given by

$$\oint_C \vec{H} \cdot d\vec{l} = I$$

where I is the current passing through the surface S enclosed by the contour C .

When using the Ampere's law, the magnetic field density vector \vec{B} should be constant along C so that we can take it outside the integral and solve the equation. Thus, the contour C should be selected carefully.

If a problem is given where we can not select such a contour, then we can not apply the Ampere's law. In such cases, integral techniques are used just as ^{we did} in the static electric field before.

The integral technique involves finding the vector magnetic potential first,

$$\vec{A} = \frac{\mu_0}{4\pi} \int_{V'} \frac{\vec{J}}{R} dV'$$

for volumetric sources.

and since $J dV' = J S dl' = I dl'$

$$A = \frac{\mu_0 I}{4\pi} \oint_{C'} \frac{dl'}{R}$$

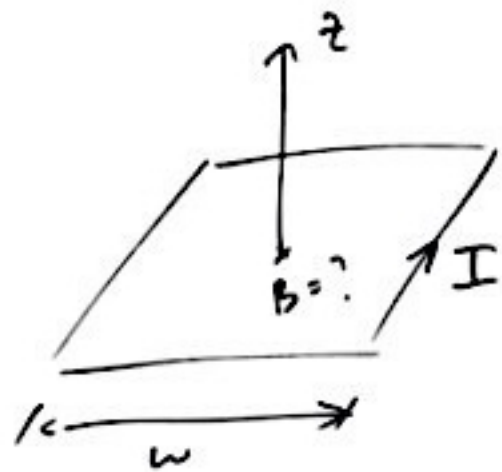
for linear sources.

Once A is obtained, the \vec{B} can be evaluated from

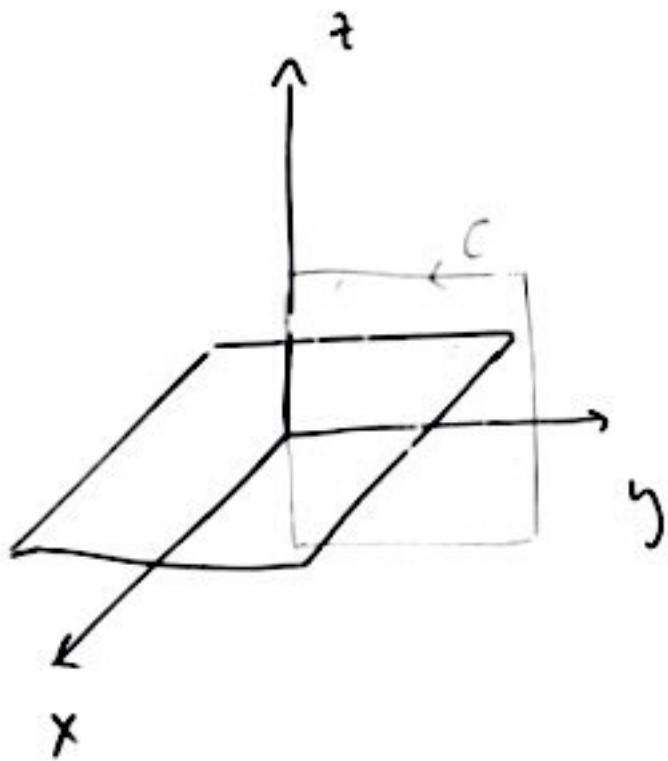
$$\vec{B} = \nabla \times \vec{A}$$

Ex:

Find the magnetic flux density vector \vec{B}
at the center of a square loop
with side w carrying a dc current I .



Ans:



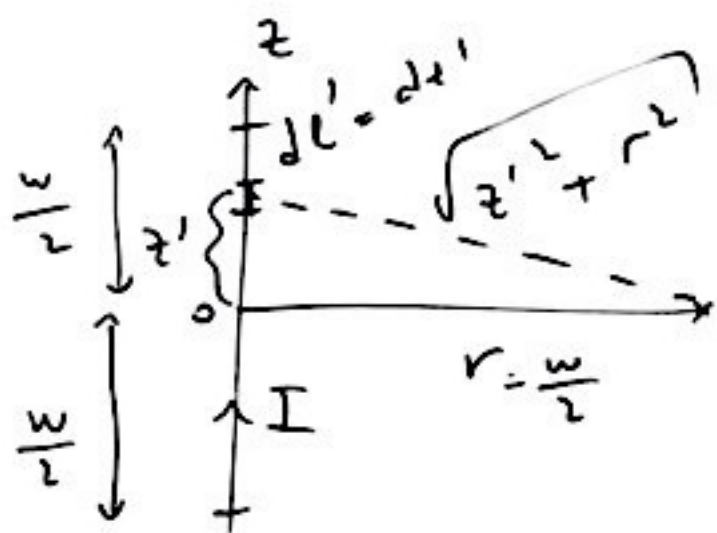
$$\int_C \vec{B} \cdot d\vec{l} = \mu_0 I$$

$$\vec{B}(x, y, z)$$

\vec{B} is a function of the
spatial (space) coord.

Hence, we can not use the
Ampere's law.

We will use the integral technique (the Biot Savart law)
 We will find \bar{A} at the center for one side only, then
 multiply by 4, due to symmetry, will yield the
 total field.



Then,

$$\bar{A} = \hat{a}_z \frac{\mu_0 I}{4\pi} \int_{-3/2}^{3/2} \frac{dz'}{\sqrt{z'^2 + r^2}}$$

or

$$\bar{A} = \hat{a}_z \frac{\mu_0 I}{4\pi} \left[\ln(z' + \sqrt{z'^2 + r^2}) \right]_{-3/2}^{3/2}$$

$$\bar{A} = \hat{a}_z \frac{\mu \cdot I}{4\pi} \ln \frac{\sqrt{\left(\frac{w}{2}\right)^2 + \left(\frac{w}{2}\right)^2} + L}{\sqrt{\left(\frac{w}{2}\right)^2 + \left(\frac{w}{2}\right)^2} - L}$$

or

$$\bar{B} = \bar{\nabla} \times \bar{A} = \bar{\nabla} \times (\hat{a}_z A_z) = \hat{a}_r \frac{1}{r} \frac{\partial A_z}{\partial \phi} - \hat{a}_\phi \frac{\partial A_z}{\partial r}$$

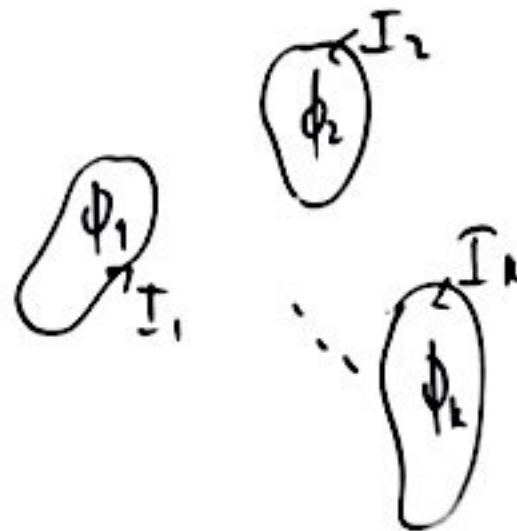
0 (due to symmetry)

$$\bar{B} = -\hat{a}_\phi \frac{\partial A_z}{\partial r} = \hat{a}_\phi \frac{\mu \cdot I \frac{w}{2}}{2\pi \frac{w}{2} \sqrt{\left(\frac{w}{2}\right)^2 + \left(\frac{w}{2}\right)^2}}$$

$$\bar{B} = h \times \bar{B} = \hat{a}_\phi \frac{4 \mu \cdot I \frac{w}{2}}{w \pi \frac{w}{2} \sqrt{2}} \left(\frac{w}{m^2} \right) /$$

Magnetic Energy:

$$W_m = \frac{1}{2} \sum_{k=1}^N I_k \phi_k$$



In terms of fields,

$$W_m = \frac{1}{2} \int_V \bar{A} \cdot \bar{J} \, dv'$$

or

$$W_m = \frac{1}{2} \int_V \bar{H} \cdot \bar{B} \, dv'$$

$$W_m = \frac{1}{2} \int_V \frac{B^2}{\mu} \, dv'$$

$$W_m = \frac{1}{2} \int_V \mu H^2 \, dv' \quad (3)$$

where

$$W_m = \frac{1}{2} \mu H^2 \left(\frac{J}{m^2} \right) \text{ is the}$$

energy density.

Cpt. 7 Time Varying Fields and Maxwell's Equations:

Faraday's law of Electromagnetic
Induction:

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

Take the Surface integral of both
sides and apply the Stoke's theorem on the
LHS.

$$\oint_C \vec{E} \cdot d\vec{l} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

A Stationary Circuit in a Time-Varying Mag. Field.

$$\oint_C \vec{E} \cdot d\vec{l} = - \frac{d}{dt} \int_S \vec{B} \cdot d\vec{s}$$

Since the circuit is stationary.

Then,

$$V = - \oint_C \vec{E} \cdot d\vec{l}$$

and

$$\phi = \int_S \vec{B} \cdot d\vec{s}$$

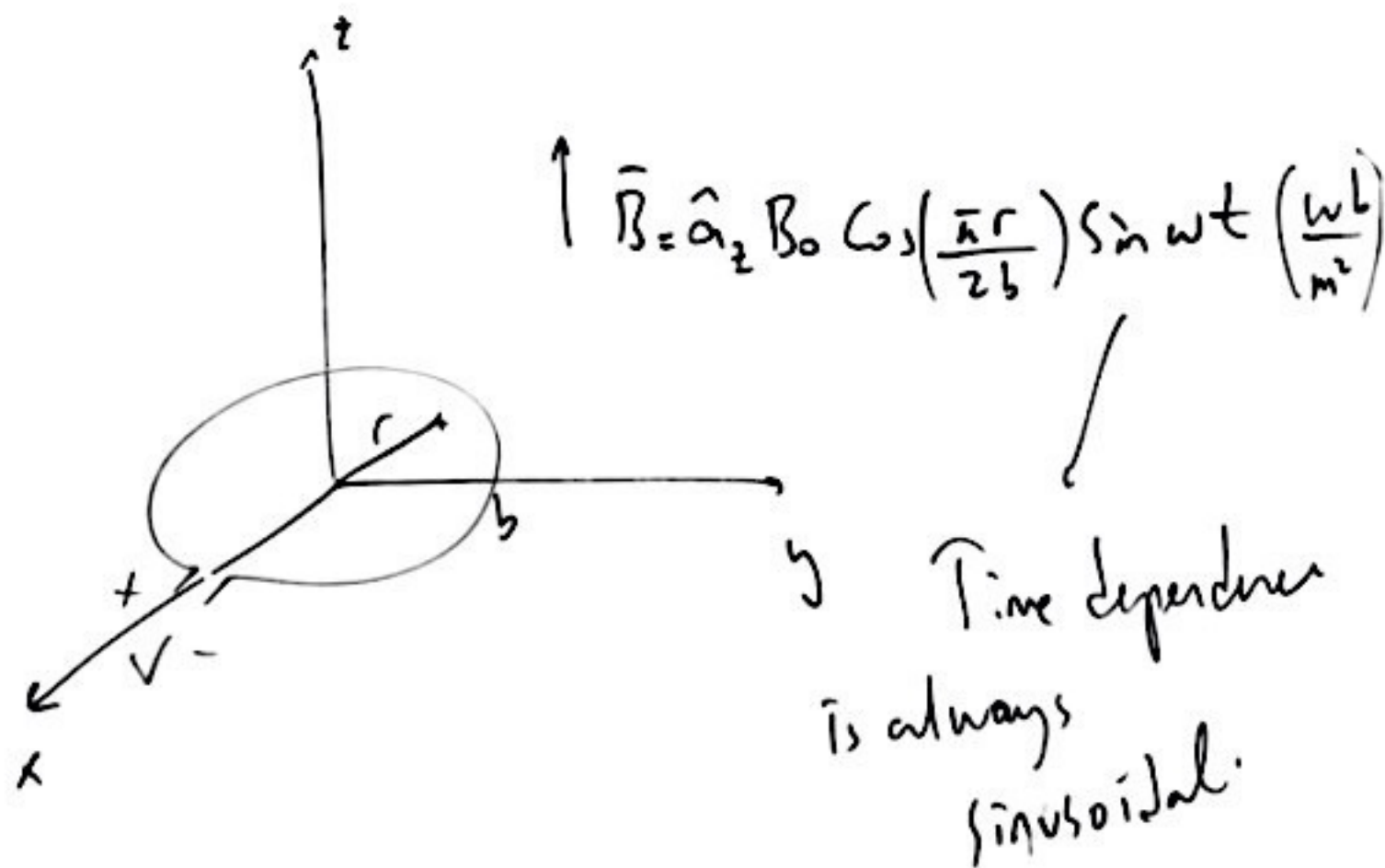
Then,

$$V = - \frac{d\phi}{dt} \quad (\text{Faraday's law of electromagnetic induction})$$

A voltage is induced in a stationary circuit which is not moving circuit

equal to the negative rate of increase in the magnetic flux linking the circuit.

Ex:



Ans!

$$\begin{aligned}\phi &= \int \vec{B} \cdot \vec{d}_1 \\ &= \int_0^b \left[\hat{a}_z B_0 \cos \omega t \frac{\pi r}{2b} \sin \omega t \right] \cdot (\hat{a}_z 2\pi r dr) \\ &= \frac{8b^2}{\pi} \left(\frac{\pi}{2} - 1 \right) B_0 \sin \omega t\end{aligned}$$

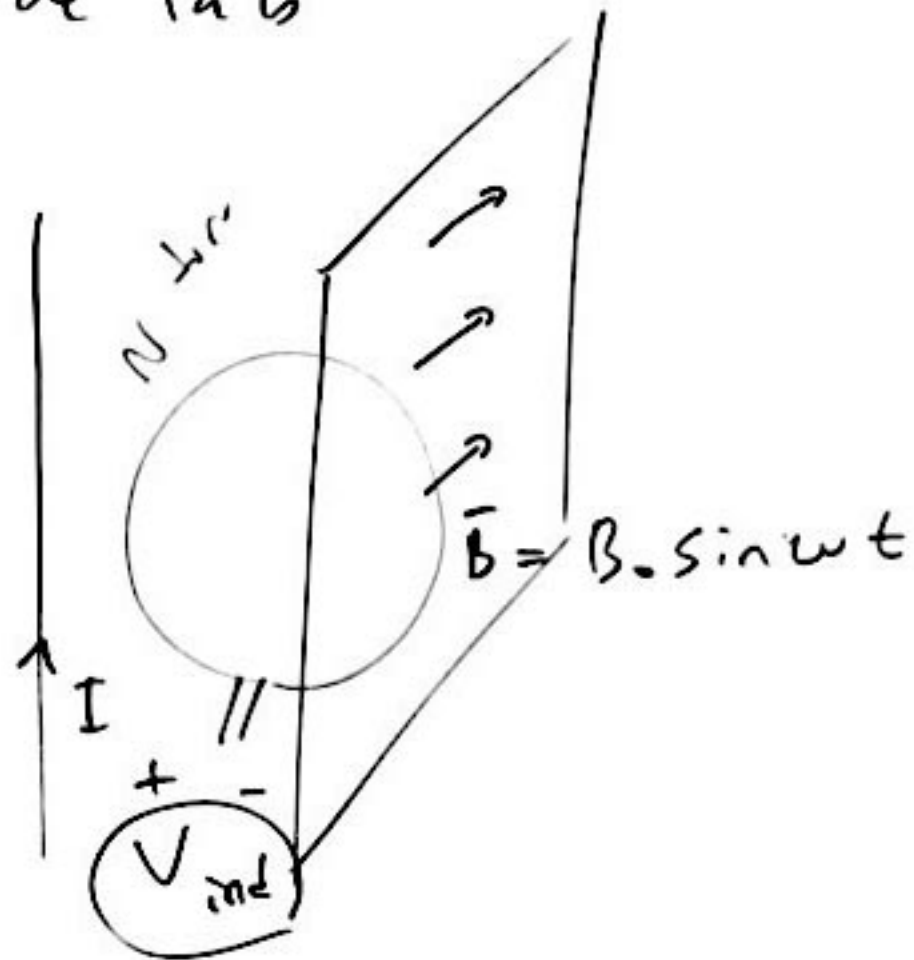
$$V = -N \cdot \frac{d\phi}{dt} \quad (\text{for } N \text{ turns})$$

$$V = -\frac{8N}{\pi} b^2 \left(\frac{\pi}{2} - 1 \right) B_0 \omega \cos \omega t \quad (v)$$

where $\omega = \text{radian frequency} = 2\pi f$

where $f = \text{Hertz freq.}$

In the lab



Take the Surface integral of both sides and apply the Stoke's theorem on the

LHS.

$$\oint_C \vec{E} \cdot d\vec{l} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$